

Multiple-Component Reactions in Optical Biosensors

¹Ryan M. Evans
David A. Edwards

University of Delaware

¹*rmevans@udel.edu*

Overview

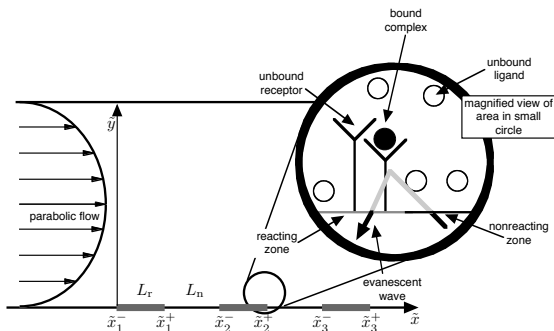
- What are optical biosensors and surface-volume reactions?
- Can we develop an accurate mathematical model for multiple-component reactions in optical biosensors?
- Given a set of data, can we determine the associated reaction rates?
- How does the reacting species behave in the single ligand case, when there exists a *strong nonlinearity* in the governing equation.

Introduction

- Many chemical reactions in biology involve a stream of chemical reactants (*ligand*) flowing through a fluid-filled volume, over a surface to which other reactants (*receptors*) are confined.
- These surface-volume reactions occur in a number of biological processes such as blood clotting, drug absorption, DNA-damage repair.

Optical Biosensor

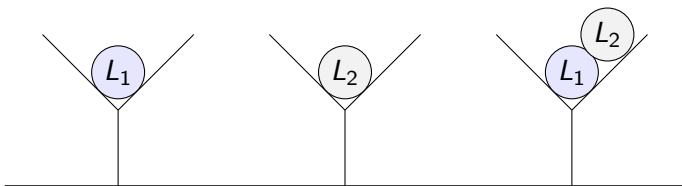
- Optical biosensors are a popular way to measure such reactions without disturbing the underlying system.



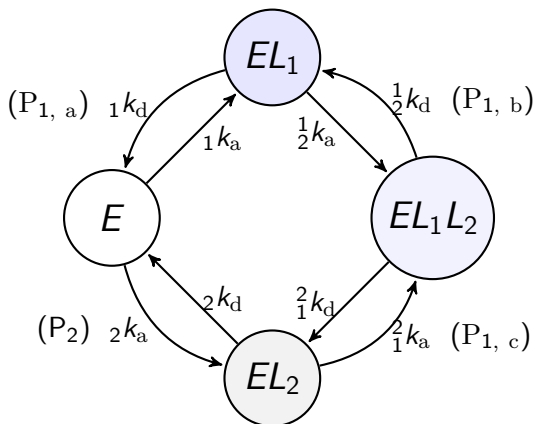
Multiple-Component Reactions

- This process has been well studied in the reaction limited, transport dominant (*weakly nonlinear*) parameter regime, when there is only a single ligand.
- What happens when there are multiple reactions on the surface?

Multiple-Component Reactions



Multiple-Component Reactions



Multiple-Component Reactions in Optical Biosensors

- Having an accurate mathematical model of this process helps interpret biosensor data.
- Biosensor only measure on a weighted average of reacting species concentrations.

Multiple-Component Reactions in Optical Biosensors

- Biosensor only measures on a weighted average of reacting species concentrations

$$S(t) := \frac{1}{x_{\max} - x_{\min}} \int_{x_{\min}}^{x_{\max}} B_1(x, t) + \left(1 + \frac{\rho_2}{\rho_1}\right) B_{12}(x, t) + \frac{\rho_2}{\rho_1} B_2(x, t) dx$$

Here B_i are reacting species concentrations

$$B_1(x, t) = [EL_1](x, t),$$

$$B_2(x, t) = [EL_2](x, t),$$

$$B_{12}(x, t) = [EL_1L_2](x, t)$$

ρ_i are molecular weights of B_i .

Multiple-Component Reactions in Optical Biosensors

- Can rewrite

$$S(t) = \frac{1}{x_{\max} - x_{\min}} \int_{x_{\min}}^{x_{\max}} B_1(x, t) + \left(1 + \frac{\rho_2}{\rho_1}\right) B_{12}(x, t) + \frac{\rho_2}{\rho_1} B_2(x, t) dx$$

more compactly as:

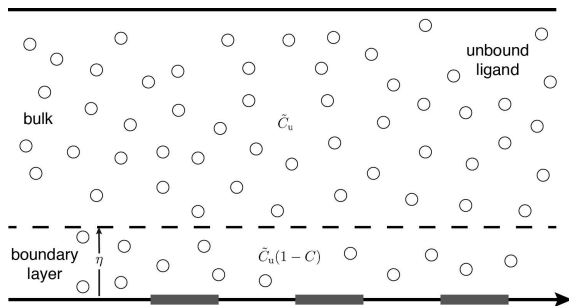
$$S(t) = \bar{B}_1(t) + \left(1 + \frac{\rho_2}{\rho_1}\right) \bar{B}_{12}(t) + \frac{\rho_2}{\rho_1} \bar{B}_2(t),$$
$$\bar{B}_i = \frac{1}{x_{\max} - x_{\min}} \int_{x_{\min}}^{x_{\max}} B_i(x, t) dx.$$

Mathematical Model

- Convection-diffusion equations for each of the unbound ligands $C_1(x, y, t) = [L_1](x, y, t)$, $C_2(x, y, t) = [L_2](x, y, t)$.
- Coupled to a system of PDE's describing the evolution of the reacting species concentration B_i at the boundary.

Two Compartment

- High flow rate and slow diffusion results means that diffusion is only important in a layer near the boundary, e.g. several time scales and boundary layers.



Mathematical Model

$$\frac{\partial C_1}{\partial t_c} = (D_r \text{Pe}^{-1}) \left(\epsilon^2 \frac{\partial^2 C_1}{\partial x^2} + \frac{\partial^2 C_1}{\partial y^2} \right) - y(1-y) \frac{\partial C_1}{\partial x}, \quad (1)$$

$$\frac{\partial C_2}{\partial t_c} = \text{Pe}^{-1} \left(\epsilon^2 \frac{\partial^2 C_2}{\partial x^2} + \frac{\partial^2 C_2}{\partial y^2} \right) - y(1-y) \frac{\partial C_2}{\partial x}. \quad (2)$$

- t_c is the convective time scale.
- $\text{Pe} \gg 1$, $\epsilon \ll 1^1$.
- D_r is the ratio of the diffusivity of the two ligands, order one.
- Parabolic velocity profile.

¹ $\text{Pe} = 3.71 \times 10^2$, $\epsilon = 2.08^{-2}$

Initial and Boundary Data

- Initial conditions: $C_j(x, y, 0) = 0$.
- Inflow condition: $C_j(0, y, t) = 1$.
- No change in the concentration as it exits the channel
 $\frac{\partial C_j}{\partial x}(1, y, t) = 0$.
- No flux through the ceiling $\frac{\partial C_j}{\partial y}(x, 1, t) = 0$.

Bottom Boundary Condition

- Diffusive flux conditions:

$$D_r D \frac{\partial C_1}{\partial y}(x, 0, t_c) = \frac{\partial B_1(x, t_c)}{\partial t_c} + \frac{\partial B_{12}(x, t_c)}{\partial t_c}$$

$$D \frac{\partial C_2}{\partial y}(x, 0, t_c) = \frac{\partial B_{12}(x, t_c)}{\partial t_c} + \frac{\partial B_2(x, t_c)}{\partial t_c}$$

- $D = \frac{\text{Diffusion rate from channel to reacting surface}}{\text{Convective Transport in Channel}}$.
- $D \ll 1 \Rightarrow$ bound state governed by slower diffusive processes.
- Need another set of equations for B_j .

Reaction Kinetics

$$\frac{\partial B_1}{\partial t_c} = {}_1k_a(1 - B_\Sigma)C_1 + {}_2k_d B_{12} - {}_1k_d B_1 - {}_1k_a B_1 C_2,$$

$$\frac{\partial B_{12}}{\partial t_c} = {}_2k_a B_1 C_2 + {}_1k_a B_2 C_1 - {}_1k_d B_{12} - {}_2k_d B_{12},$$

$$\frac{\partial B_2}{\partial t_c} = {}_2k_d B_{12} + {}_2k_a(1 - B_\Sigma)C_2 - {}_1k_a B_2 C_1 - {}_2k_d B_2,$$

$$B_\Sigma = B_1 + B_{12} + B_2$$

- $1 - B_\Sigma$ empty receptor concentration
- Initially no bound ligand $B_1(x, 0) = B_{12}(x, 0) = B_2(x, 0) = 0$,

Reaction Kinetics

$$\frac{\partial B_1}{\partial t_c} = {}_1k_a(1 - B_\Sigma)C_1 + {}_2k_d B_{12} - {}_1k_d B_1 - {}_2k_a B_1 C_2, \quad (3)$$

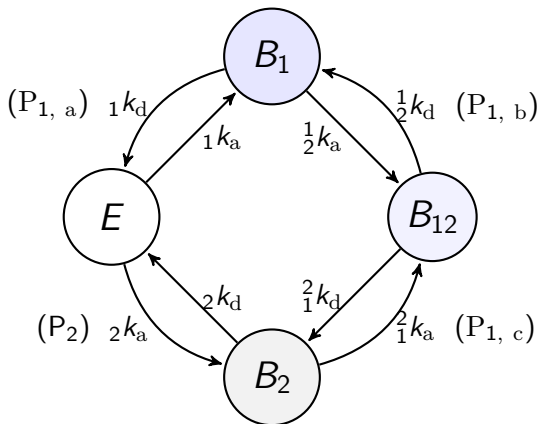
$$\frac{\partial B_{12}}{\partial t_c} = {}_2k_a B_1 C_2 + {}_1k_a B_2 C_1 - {}_1k_d B_{12} - {}_2k_d B_{12}, \quad (4)$$

$$\frac{\partial B_2}{\partial t_c} = {}_2k_d B_{12} + {}_2k_a(1 - B_\Sigma)C_2 - {}_2k_d B_2 - {}_1k_a B_2 C_1, \quad (5)$$

$$B_\Sigma = B_1 + B_{12} + B_2 \quad (6)$$

- $1 - B_\Sigma$ empty receptor concentration
- Initially no bound ligand $B_1(x, 0) = B_{12}(x, 0) = B_2(x, 0) = 0$,

Multiple-Component Reactions



Reaction Kinetics

- Adding these three equations we find

$$\frac{\partial B_{\Sigma}}{\partial t} = {}_1k_a(1 - B_{\Sigma}) + {}_2k_a(1 - B_{\Sigma}) - {}_1k_d B_1 - {}_2k_d B_2 \quad (7)$$

- The only change in the total ligand concentration is due to association/dissociation.

Bulk Compartment

- We can think of Pe^{-1} as a perturbation parameter and use the fact that $D \ll 1$ to arrive at the leading order equations:

$$\frac{\partial C_i}{\partial t_c} = -y(1-y) \frac{\partial C_i}{\partial x}, \quad (8)$$

$$C_i(0, y, t_c) = 1, \quad (9)$$

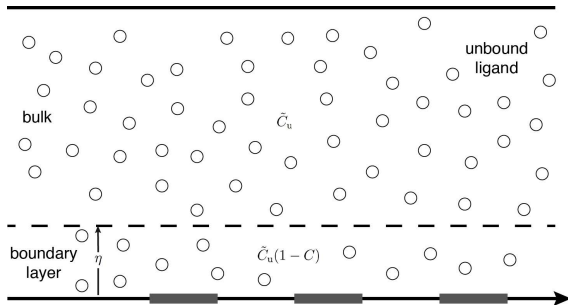
$$C_i(x, y, 0) = 0, \quad (10)$$

$$0 = \frac{\partial B_1}{\partial t_c} + \frac{\partial B_{12}}{\partial t_c}, \quad (11)$$

$$0 = \frac{\partial B_{12}}{\partial t_c} + \frac{\partial B_2}{\partial t_c}. \quad (12)$$

Two Compartment

- Compartment model



Diffusive Layers

- There may be discontinuity between the solution in the bulk compartment and the solution in the boundary layer.
- To fix this one would introduce an intermediate (*diffusive layer*) to smooth out any discontinuities.
- But the reaction dynamics do not occur *on this time scale*, so we will not concern ourselves with including such layers.

Unstirred Layer on the Reactive Time Scale

- Diffusion in the vertical direction balances with convection in the x direction.

$$D_r \frac{\partial^2 C_1}{\partial \eta^2} = \eta \frac{\partial C_1}{\partial x},$$
$$C_1(0, \eta, t) = 1.$$

- Here $\eta = \text{Pe}^{1/3} y$ is the stretched layer coordinate.
- Change completely driven by reaction at the boundary.
- As we exit the layer, the concentration in the unstirred layer must match the uniform outer concentration $C(x, \infty, t) = 1$

Unstirred Layer

- Diffusive flux condition

$$D_r \frac{\partial C_1}{\partial \eta}(x, 0, t) = \text{Da} \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) \quad (13)$$

- Da is the *Damköhler Number*, and represents the ratio of reaction to diffusion.
- $\text{Da} \ll 1$ for most reactions, *key perturbation parameter*.

Reaction Kinetics

- Need to get C_i in terms of B_j .

$$\frac{\partial B_1}{\partial t} = {}_1k_a(1 - B_\Sigma)C_1 + \frac{1}{2}k_d B_{12} - {}_1k_d B_1 - \frac{1}{2}k_a B_1 C_2,$$

$$\frac{\partial B_{12}}{\partial t} = \frac{1}{2}k_a B_1 C_2 + \frac{2}{1}k_a B_2 C_1 - \frac{1}{2}k_d B_{12} - \frac{2}{1}k_d B_{12},$$

$$\frac{\partial B_2}{\partial t} = \frac{2}{1}k_d B_{12} + {}_2k_a(1 - B_\Sigma)C_2 - \frac{2}{1}k_a B_2 C_1 - {}_2k_d B_2.$$

Unstirred Layer

- Consider the set of PDE's for C_1

$$D_r \frac{\partial^2 C_1}{\partial \eta^2} = \eta \frac{\partial C_1}{\partial x} \quad (14)$$

$$D_r \frac{\partial C_1}{\partial \eta}(x, 0, t) = \text{Da} \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right), \quad (15)$$

- Introduce a Laplace transform in x in (14) and use (15):

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}.$$

Ligand Depletion

- Convolution integral represents upstream ligand depletion

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}$$

- Ligand concentration a perturbation away from the outer concentration.
- Defined as

$$J^\alpha f(x) = \int_0^x f(\nu) \frac{d\nu}{(x - \nu)^{1-\alpha}}, \quad (16)$$

one may recognize the integral term in C_1 as a fractional integral, with $\alpha = 1/3$.

Bound State System

- The bound state system is then:

$$\frac{\partial B_1}{\partial t} = (1 - B_\Sigma)C_1 - {}_1K_d B_1 - \frac{1}{2}K_a B_1 C_2 + \frac{1}{2}K_d B_{12}$$

$$\frac{\partial B_{12}}{\partial t} = \frac{1}{2}K_a B_1 C_2 - \frac{1}{2}K_d B_{12} + \frac{2}{1}K_a B_2 C_1 - \frac{2}{1}K_d B_{12}$$

$$\frac{\partial B_2}{\partial t} = \frac{2}{1}K_d B_{12} - \frac{2}{1}K_a B_2 C_1 + {}_2K_a(1 - B_\Sigma)C_2 - {}_2K_d B_2$$

with

$$C_1(x, 0, t) = 1 - \frac{Da}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}$$

$$C_2(x, 0, t) = 1 - \frac{Da}{3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}$$

Perturbation Approximation

- $Da \ll 1$, so we can search for a perturbation expansion of the form

$$\mathbf{B} = {}^0\mathbf{B} + Da^1\mathbf{B} + O(Da^2). \quad (17)$$

- Leading order:

$$\frac{d^0\mathbf{B}}{dt} = -A^0\mathbf{B} + \mathbf{e}_1 + {}_2K_a\mathbf{e}_3 \quad (18)$$

$${}^0\mathbf{B}(t) = (I - e^{-At})[A^{-1}(\mathbf{e}_1 + {}_2K_a\mathbf{e}_3)], \quad (19)$$

e.g. well mixed approximation.

- The spatial dependence in ${}^1\mathbf{B}(x, t) \sim x^{1/3}$.

Perturbation Approximation

- Thus we may write

$$\mathbf{B}(x, t) = (I - e^{-At})[A^{-1}(\mathbf{e}_1 + {}_2K_a + x^{1/3}\text{Da}^1\mathbf{B}(t))] + O(\text{Da}^2). \quad (20)$$

- Problem: ${}^1\mathbf{B}$ contains a secular term of the form $te^{-\lambda t}$ in one of its components.
- A multiple scale expansion would be unweildy, and would have to be manipulated again to obtain an expression of physical relevance.

Another Approximation

- We are really interested in $\bar{\mathbf{B}}$.
- What if we could derive a set of equations for $\bar{\mathbf{B}}$, and solve them numerically using a standard ODE Package?

Averaged Bound State System

- To do this we would integrate both sides of

$$\frac{\partial B_1}{\partial t} = (1 - B_\Sigma)C_1 - {}_1K_d B_1 - \frac{1}{2}K_a B_1 C_2 + \frac{1}{2}K_d B_{12}$$

$$\frac{\partial B_{12}}{\partial t} = \frac{1}{2}K_a B_1 C_2 - \frac{1}{2}K_d B_{12} + \frac{2}{1}K_a B_2 C_1 - \frac{2}{1}K_d B_{12}$$

$$\frac{\partial B_2}{\partial t} = \frac{2}{1}K_d B_{12} - \frac{2}{1}K_a B_2 C_1 + {}_2K_a(1 - B_\Sigma)C_2 - {}_2K_d B_2$$

using

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}},$$

$$C_2(x, 0, t) = 1 - \frac{\text{Da}}{3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}.$$

How to Deal With Convolution Integral

- We may exploit the fact that to leading order B is independent of space

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}$$

$$B_1(x, t) = {}^0B_1(t) + \text{Da}^1 B_1(x, t) + O(\text{Da}^2)$$

- By substituting our expansion into C_1 we arrive at

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{d^0 B_1}{dt} + \frac{d^0 B_{12}}{dt} \right) (t) \frac{d\nu}{(x - \nu)^{2/3}} + O(\text{Da}^2)$$

How to Deal With Convolution Integral

- Since time dependence factors out of the integral, we may write

$$C_1(x, 0, t) = 1 - Da h(x) \left(\frac{d^0 B_1}{dt} + \frac{d^0 B_{12}}{dt} \right) + O(Da^2) \quad (21)$$

where,

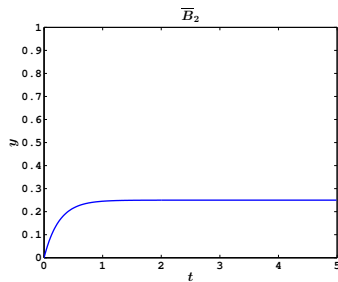
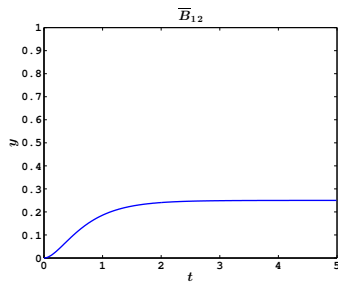
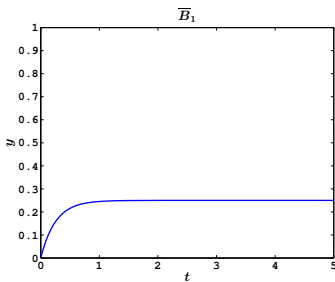
$$h(x) = \frac{1}{3^{1/3} \Gamma(2/3)} \int_0^x (x - \nu)^{-2/3} d\nu = \frac{3^{2/3} x^{1/3}}{\Gamma(2/3)}. \quad (22)$$

ERC Equations

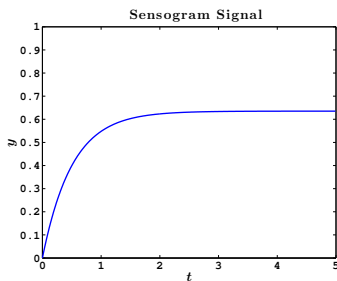
- Using these manipulations and some algebra we can derive a set of nonlinear ODE's, *Effective Rate Constant Equations*, for $\bar{\mathbf{B}}$:

$$\frac{d\bar{\mathbf{B}}}{dt} = (I + DaN(\bar{\mathbf{B}}))^{-1}(-A\bar{\mathbf{B}} + \mathbf{e}_1 + {}_2K_a\mathbf{e}_3) + \mathcal{O}(Da^2).$$

ERC Equation Solution



ERC Equation Solution



- $Da = .01$.
- Reaction rates equal to one.

Numerics

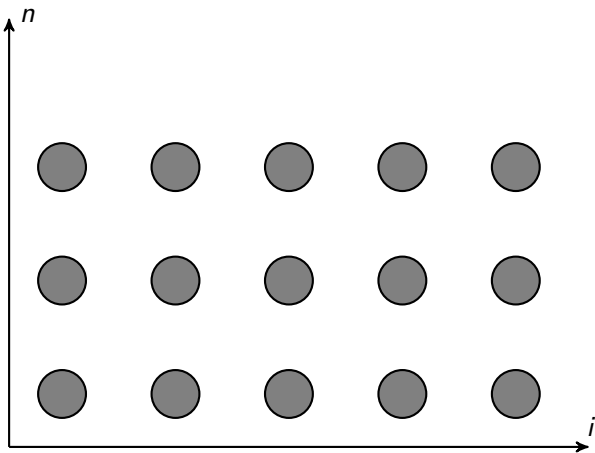
- Used a finite difference algorithm

$$\frac{\partial B_{i,n+1}^1}{\partial t} = (1 - B_{i,n}^\Sigma) C_{i,n+1}^1 - {}_1K_d B_{i,n}^1 - {}_2K_a B_{i,n}^1 C_{i,n+1}^2 + {}_2K_d B_{i,n}^{12},$$

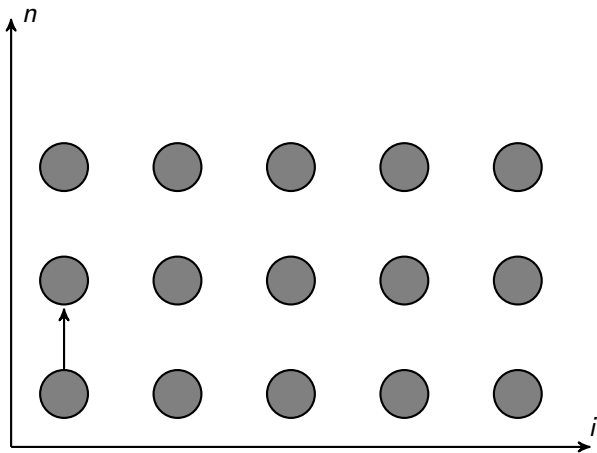
$$\frac{\partial B_{i,n+1}^{12}}{\partial t} = {}_2K_a B_{i,n}^2 C_{i,n+1}^2 - {}_2K_d B_{i,n}^{12} + {}_1K_a B_{i,n}^2 C_{i,n+1}^1 - {}_1K_d B_{i,n}^{12},$$

$$\frac{\partial B_{i,n+1}^2}{\partial t} = {}_1K_d B_{i,n}^{12} - {}_1K_a B_{i,n}^2 C_{i,n+1}^1 + {}_2K_a (1 - B_{i,n}^\Sigma) C_{i,n+1}^2 - {}_2K_d B_{i,n}^2.$$

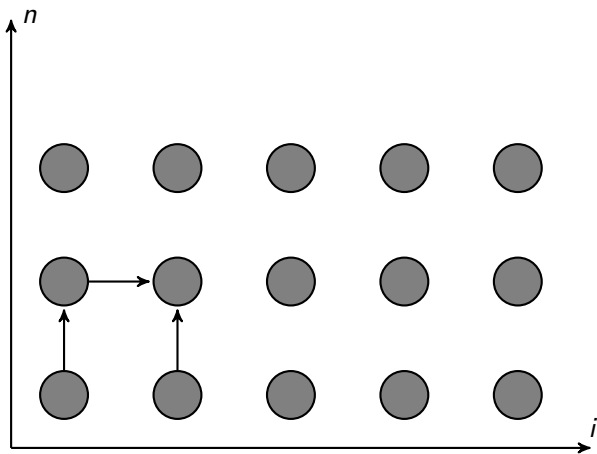
Multiple-Component Reactions



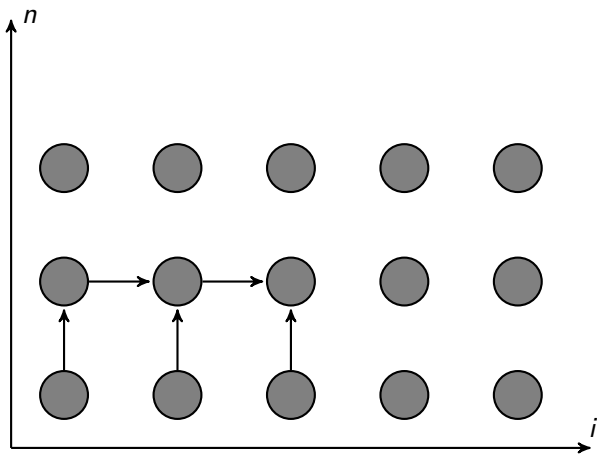
Multiple-Component Reactions



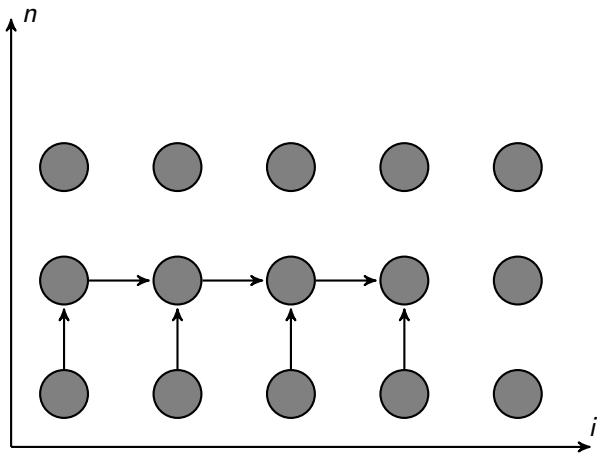
Multiple-Component Reactions



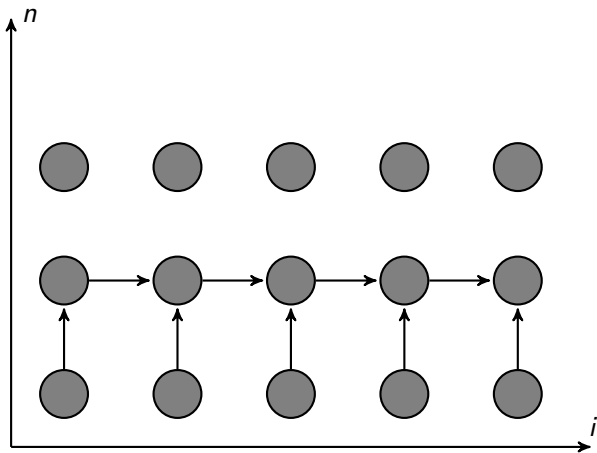
Multiple-Component Reactions



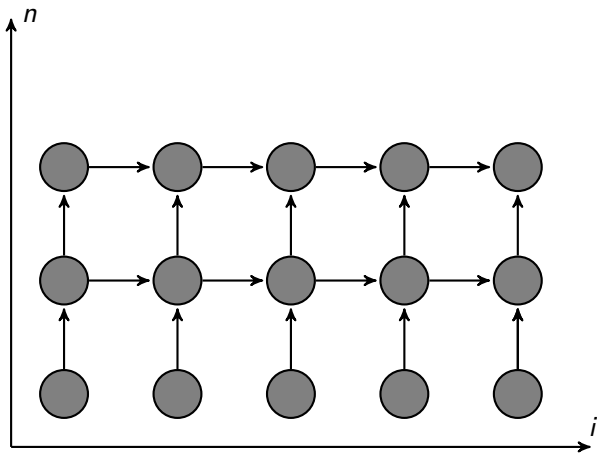
Multiple-Component Reactions



Multiple-Component Reactions



Multiple-Component Reactions



Singular Convolution Integral

- Difficult to deal with singularity

$$C_{i,n+1}^1 = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^{x_i} \left(\frac{\partial B_1}{\partial t}(x_i - \xi, t_{n+1}) + \frac{\partial B_{12}}{\partial t}(x_i - \xi, t_{n+1}) \right) (\nu, t) \frac{d\xi}{\xi^{-2/3}}$$

- Use trapezoidal rule to discretize the integral

Convolution Integral

- Subtract out the singularity

$$C_{i,n+1}^1 = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \left[\int_0^{x_i} \left(\frac{\partial B_1}{\partial t}(x_i - \xi, t_{n+1}) - \frac{\partial B_{i,n+1}^1}{\partial t} + \frac{\partial B_{12}}{\partial t}(x_i - \xi, t_{n+1}) - \frac{\partial B_{i,n+1}^{12}}{\partial t} \frac{d\xi}{\xi^{-2/3}} \right) + 3x_i^{1/3} \left(\frac{\partial B_{i,n+1}^1}{\partial t} + \frac{\partial B_{i,n+1}^{12}}{\partial t} \right) \right]$$

- Even when singularity is subtracted out, convergence is only $O(\Delta x^{2/3})$ due to functional form.
- Temporal convergence $O(\Delta t^2)$, from AB2 time-stepping scheme.

Results

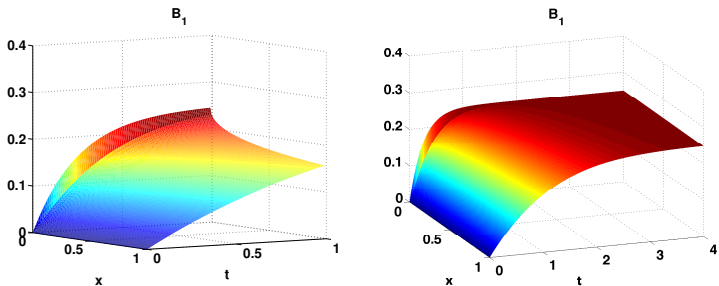
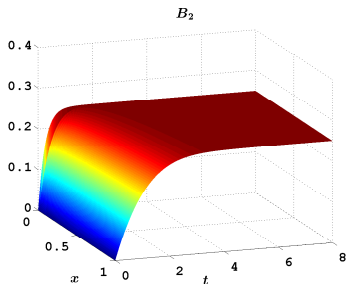
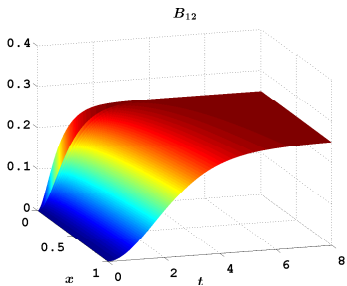
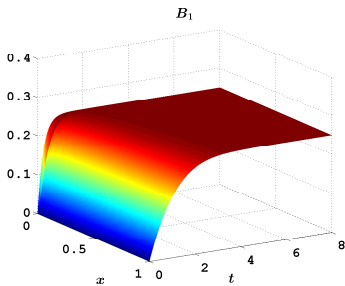


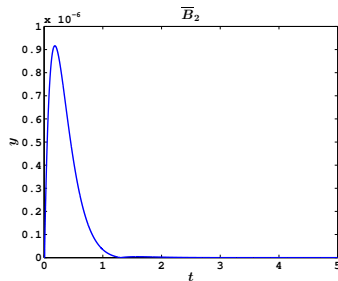
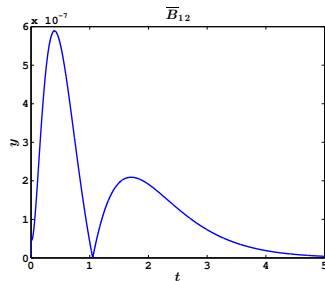
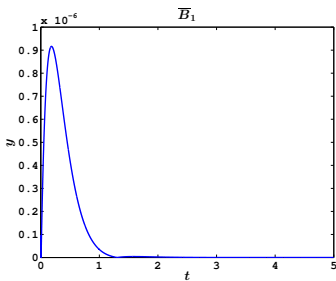
Figure : Left: B_1 after 1 second. Right: B_1 after 5 seconds

- $Da = 2$.
- All reaction rate constants taken to be 1

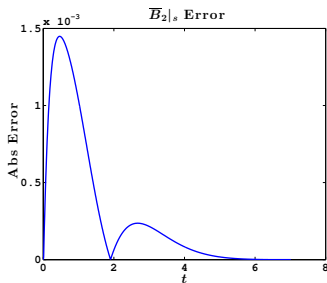
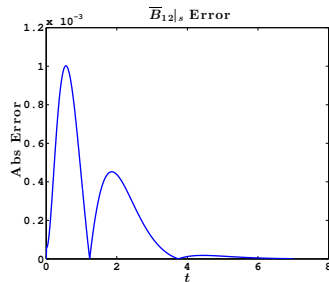
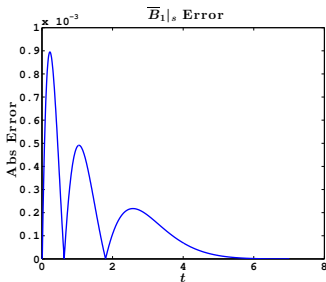
Results



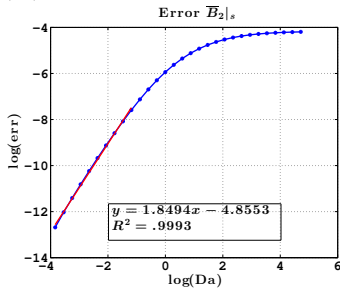
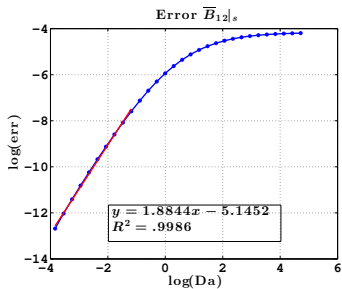
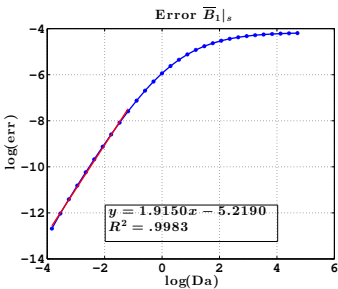
Error in ERC Equations



Error in ERC Equations



ERC Error vs Da



Wash Phase

- We have derived similar results for the wash phase.
- Recall in the wash phase, only the buffer fluid is flowing through the biosensor.

Wash Phase

- In this case, we still have the same kinetics system at the boundary,

$$\frac{\partial B_1}{\partial t} = (1 - B_\Sigma)C_1 - {}_1K_d B_1 - \frac{1}{2}K_a B_1 C_2 + \frac{1}{2}K_d B_{12},$$

$$\frac{\partial B_{12}}{\partial t} = \frac{1}{2}K_a B_1 C_2 - \frac{1}{2}K_d B_{12} + \frac{2}{1}K_a B_2 C_1 - \frac{2}{1}K_d B_{12},$$

$$\frac{\partial B_2}{\partial t} = \frac{2}{1}K_d B_{12} - \frac{2}{1}K_a B_2 C_1 + {}_2K_a(1 - B_\Sigma)C_2 - {}_2K_d B_2.$$

- Unbound ligand concentration at the surface will be different, *i.e.* only trace amounts.

Wash Phase

- Therefore instead of

$$C_1(x, 0, t) = 1 - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}},$$

we have

$$C_1(x, 0, t) = - \frac{\text{Da}}{D_r^{2/3} 3^{1/3} \Gamma(\frac{2}{3})} \int_0^x \left(\frac{\partial B_1}{\partial t} + \frac{\partial B_{12}}{\partial t} \right) (\nu, t) \frac{d\nu}{(x - \nu)^{2/3}},$$

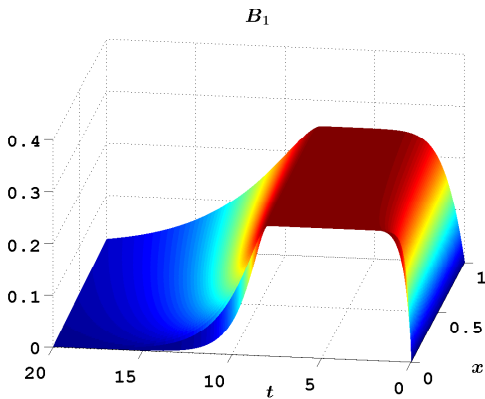
- In this case $\frac{\partial B_i}{\partial t} < 0$, and $C_1 = O(\text{Da})$.

Wash Phase Results

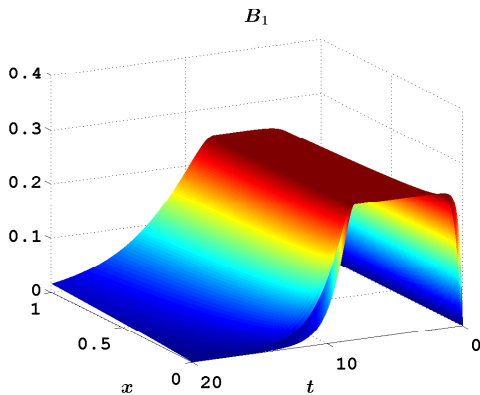
- ERC equations in this case are

$$\frac{d\bar{\mathbf{B}}}{dt} = (I + DaN(\bar{\mathbf{B}}))^{-1}(-D\bar{\mathbf{B}}) + O(Da^2) \quad (23)$$

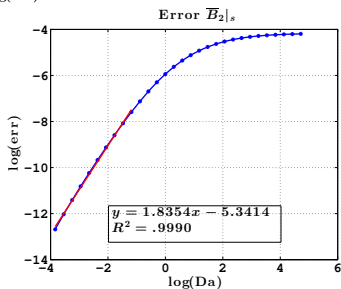
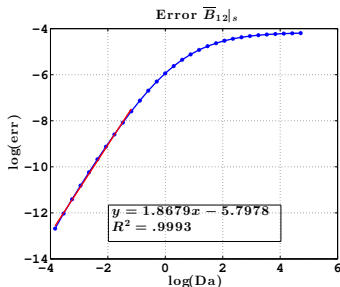
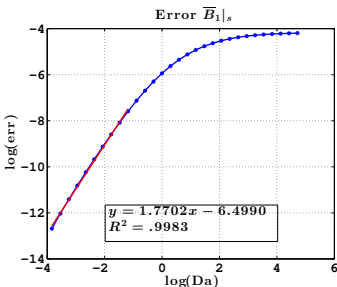
Wash Phase Results: FD Solution



Wash Phase Results: FD Solution



Wash Phase Results: ERC Error vs. Da



Recovering Reaction Rates

- Overall Goal: What are the reaction rates?
 - Can we actually find cases where **different rate constants give the same signal?**
 - Can we develop a curve fitting algorithm?

Recovering Reaction Rates

- Take $Da = 0$ and study the linear set of ODE's

$$\frac{d\mathbf{B}}{dt} = -\mathbf{A}\mathbf{B} + \mathbf{f}, \quad \mathbf{B}(0) = \mathbf{0}. \quad (24)$$

- Use (24) as our data.

Recovering Reaction Rates

- Here

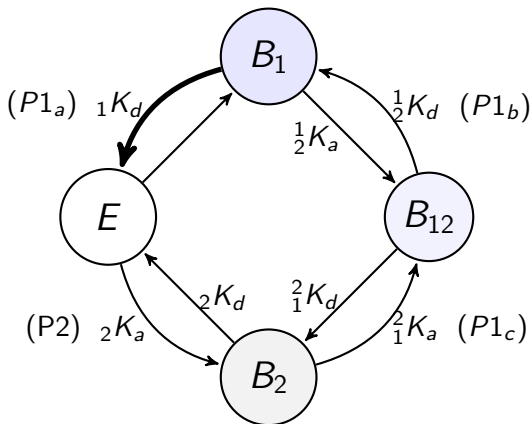
$$A = \begin{pmatrix} (1 + {}_1K_d + \frac{1}{2}K_a) & 1 - \frac{1}{2}K_d & 1 \\ -\frac{1}{2}K_a & (\frac{1}{2}K_d + \frac{2}{1}K_d) & -\frac{2}{1}K_a \\ {}_2K_a & {}_2K_a - \frac{2}{1}K_d & ({}_2K_a + {}_2K_d + \frac{2}{1}K_a) \end{pmatrix}$$

and $\mathbf{f} = \mathbf{e}_1$ or $\mathbf{f} = {}_2K_a\mathbf{e}_3$

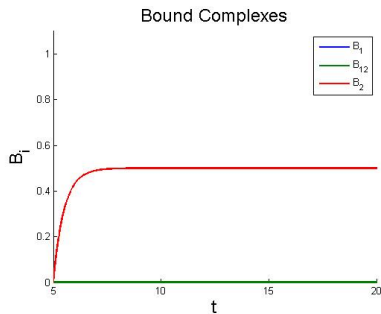
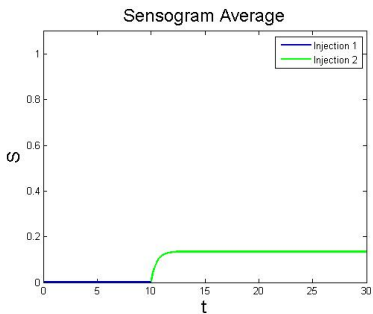
Methodology

- First inject ligand one until the system reaches an equilibrium, then inject ligand two.
- Broke the problem up into cases based on the size of ${}_1K_d$, ${}_2K_a$, ${}_2K_d$.

Recovering Reaction Rates

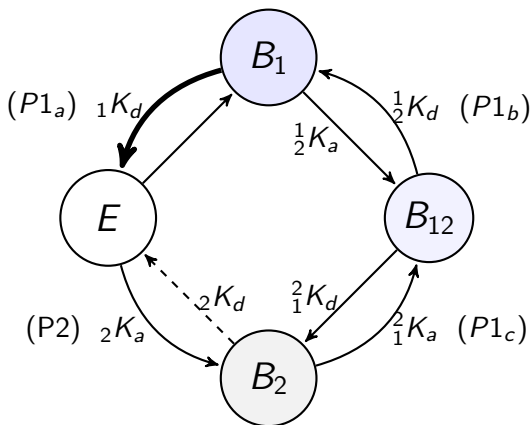


Recovering Reaction Rates

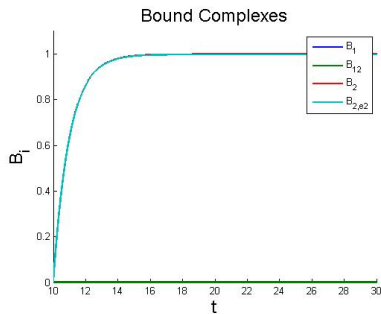
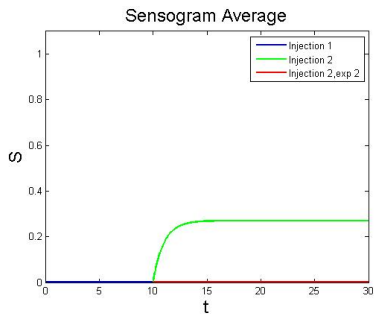


- ${}_1K_d = 100$

Recovering Reaction Rates

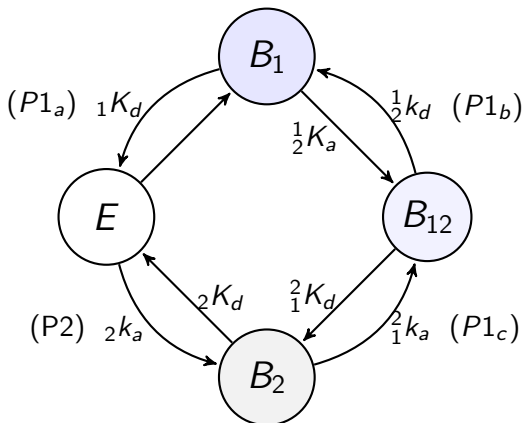


Recovering Reaction Rates

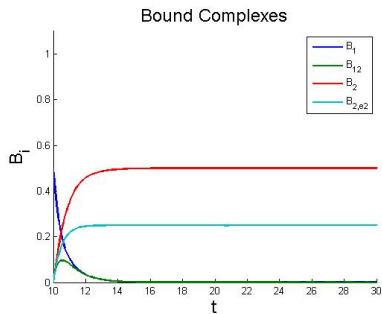
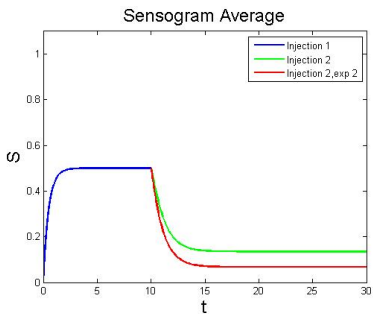


- ${}_1K_d = 100, {}_2K_d = \frac{1}{100}$

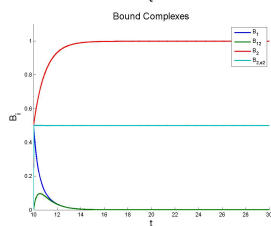
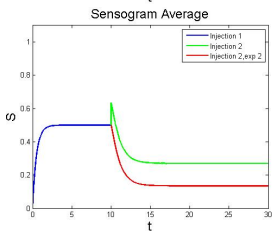
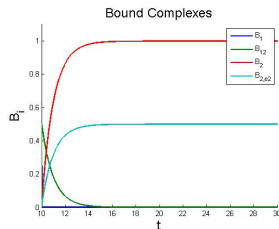
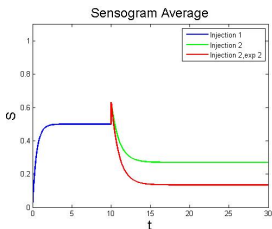
Recovering Reaction Rates



Recovering Reaction Rates

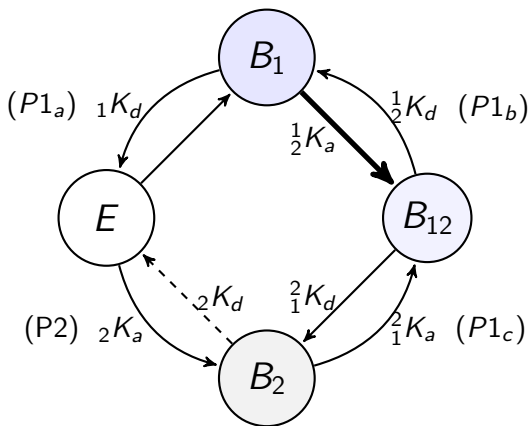


Ambiguous Sensogram

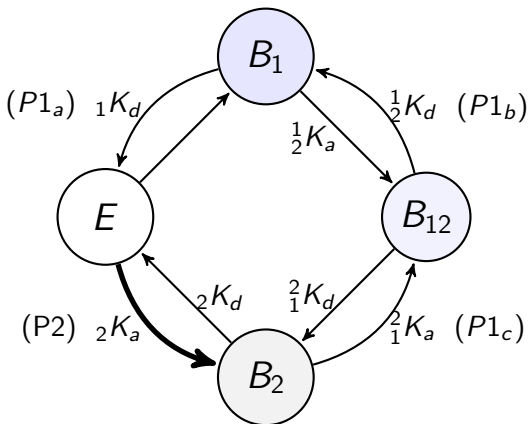


- Left: ${}_2K_d = 100$, ${}_1K_a = \frac{1}{100}$. Right: ${}_2K_a = 100$. Both: $C_1 = 1$.

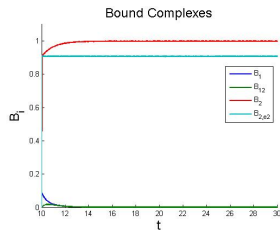
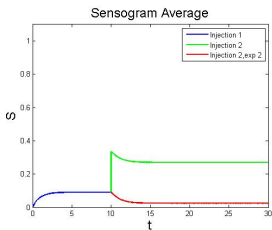
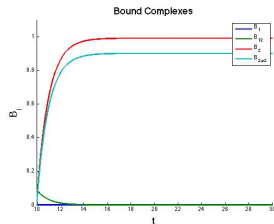
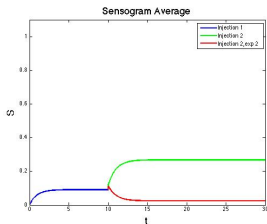
Ambiguous Sensogram: Case 1



Ambiguous Sensogram: Case 2



Clarified Sensogram



- Left: ${}_2K_d = \frac{1}{100}$, $\frac{1}{2}K_a = 100$. Right: ${}_2K_a = 100$. Both: $C_1 = .1$.

Single Ligand Analysis

- When studying the single ligand process, there is only one type of reaction at the boundary.
- In this case the reacting species concentration obeys the equation

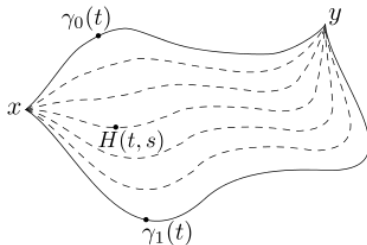
$$\frac{\partial B}{\partial t} = (1 - B) \left(1 - \frac{\text{Da}}{3^{1/3}\Gamma(2/3)} \int_0^x \frac{\partial B}{\partial t}(\nu, t) \frac{d\nu}{(x - \nu)^{2/3}} \right) - KB$$

- Can we find an analytic expression for B or \bar{B} when $\text{Da} = O(1)$?

A Homotopy Method

- *Homotopy*: a continuous deformation of one curve into another.

$$\mathcal{H}(t, s) = (1 - s)\gamma_0(t) + s\gamma_1(t), \quad s \in [0, 1]$$



- Can we try the same thing with differential operators?

A Homotopy of Differential Operators

- Many differential operators \mathcal{A} can be composed into a linear part \mathcal{L} , and nonlinear part \mathcal{N}

$$\underbrace{\mathcal{L}(B) + \mathcal{N}(B)}_{\mathcal{A}(B)} = \mathcal{F}. \quad (25)$$

- We can draw a homotopy between \mathcal{L} and \mathcal{A}

$$\mathcal{H}(B, p) = (1 - p)\mathcal{L}(B) + p\mathcal{A}(B), \quad p \in [0, 1]. \quad (26)$$

Nuts and Bolts

- Therefore we can propose a series solution to

$$\begin{aligned}\mathcal{H}(B, p) &= 1 \\ \Leftrightarrow (1 - p)\mathcal{L}(B) + p\mathcal{A}(B) &= \mathcal{F}, \quad p \in [0, 1].\end{aligned}$$

of the form

$$B(x, t) = B_0(x, t) + pB_1(x, t) + p^2B_2(x, t) + \dots$$

Nuts and Bolts

- Thus when examining the p^{th} coefficient of our series in the equation

$$\Leftrightarrow (1 - p)\mathcal{L}(B) + p\mathcal{A}(B) = \mathcal{F}, \quad p \in [0, 1]. \quad (27)$$

we will find that the nonlinearity is higher order.

- That is we will have an equation of the form

$$\mathcal{L}(B_i) = -\mathcal{N}(B_1, \dots, B_{i-1}). \quad (28)$$

Single Ligand Analysis

- The equation governing the bound state in the single ligand case is

$$\frac{\partial B}{\partial t} = (1 - B) \left(1 - \frac{\text{Da}}{3^{1/3}\Gamma(2/3)} \int_0^x \frac{\partial B}{\partial t}(\nu, t) \frac{d\nu}{(x - \nu)^{2/3}} \right) - KB$$

- First we obtain an expression for \bar{B} by averaging each side, and rearranging some terms:

$$\underbrace{\frac{d\bar{B}}{dt} + (1 + K)\bar{B}}_{\mathcal{L}} + \underbrace{\frac{\text{Da}}{3^{1/3}\Gamma(2/3)} (B - 1) \int_0^x \frac{\partial B}{\partial t}(\nu, t) \frac{d\nu}{(x - \nu)^{2/3}}}_{\mathcal{N}} = 1$$

Series Solution

- Propose and substitute a series solution.

$$B(x, t) = B_0(x, t) + pB_1(x, t) + p^2B_{12}(x, t) + \dots \quad (29)$$

$$\mathcal{H}(B, p) = 1. \quad (30)$$

- Get linear ODE's for $\bar{B}_0(t)$, $\bar{B}_1(t)$, $\bar{B}_2(t)$, ...
- An approximation to \bar{B} is then given by

$$\bar{B}(t) = \bar{B}_0 + \bar{B}_1(t) + \bar{B}(t) + \dots$$

Two Terms

- Doing this the first two terms are:

$$B_0(t) = \alpha^{-1}(1 - e^{-\alpha t})$$

$$B_1(t) = -\frac{Da\bar{h}e^{-2t\alpha}(-1 + e^{t\alpha} - e^{t\alpha}t\alpha + e^{t\alpha}t\alpha^2)}{\alpha^2}$$

$$\alpha = (K + 1)$$

$$\bar{h} = \frac{\overline{x^{1/3}}}{3^{1/3}\Gamma(2/3)}$$

Issues

- **Convergence** of our series.
 - When $Da = O(1)$ or $Da \gg 1$, what guarantees that our series will converge?
- **Secular term** of the form $te^{-\alpha t}$
 - This is not bad enough make our series converge, but still throws off the accuracy.

Convergence

- A standard technique is to embed a convergence control parameter q into our homotopy

$$(1 - p)(\mathcal{L}(\bar{B}) - \mathcal{L}(b_0)) + qp\mathcal{A}(B) = 1, \quad p \in [0, 1]. \quad (31)$$

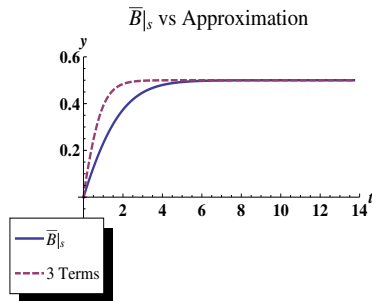
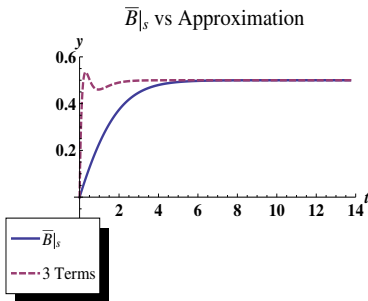
- Choose q that minimizes

$$\|\mathcal{A}(B) - 1\|_2^2 \quad (32)$$

- Done numerically in Mathematica.

Time Scale

- We can fix convergence, but the *time scale* is still off.



- $Da = 3$; This is a 3 term approximation with and without the convergence parameter q

Time Scale

- The propose a strained time scale of the form:

$$\tau = (1 + p\omega_1 + p^2\omega_2 + \dots)t, \quad (33)$$

where the ω_i are choosen to eliminate secular terms.

Expansion

- The first two terms are:

$$\bar{B}_0(\tau) = \alpha^{-1}(1 - e^{-\alpha\tau}),$$

$$\bar{B}_1(\tau; q) = \frac{qDa\bar{h}e^{-2\alpha\tau}(e^{\alpha\tau} - 1)}{\alpha^2},$$

$$\tau = (1 + \omega_1 + \omega_2 + \dots)t,$$

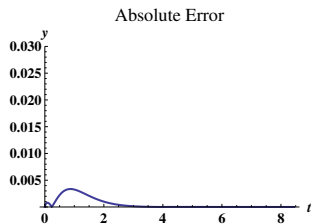
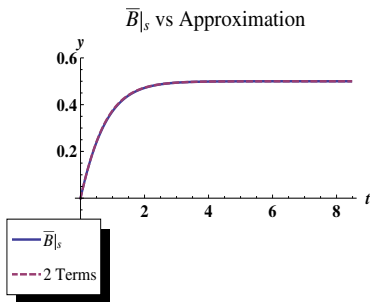
where $\alpha = (1 + K)$, and

$$\omega_1 = -qDa\bar{h}(1 - \alpha^{-1}),$$

$$\omega_2 = Da\bar{h}q\alpha^{-2}(\alpha - 1)(-Da\bar{h}q + \alpha - q\alpha + Da\bar{h}q\alpha),$$

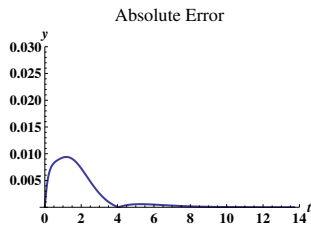
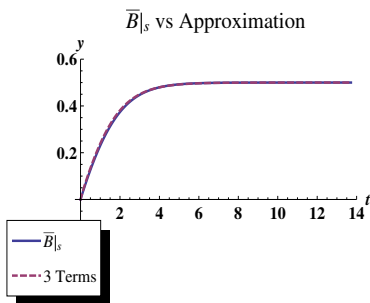
$$\bar{h} = \frac{\bar{x}^{1/3}}{3^{1/3}\Gamma(2/3)}.$$

Two Term Expansion, $Da = 1/2$



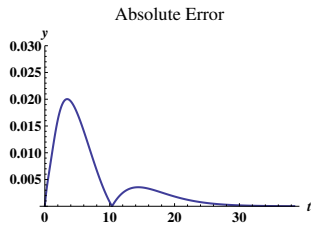
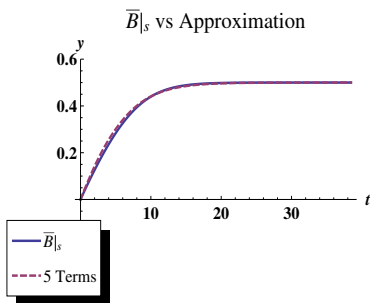
- Two term expansion, $Da = 1/2$.

Three Term Expansion, $Da = 2$



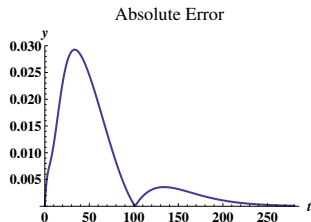
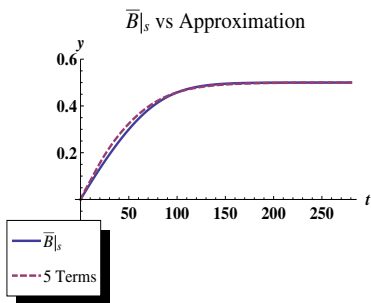
- Three term Approximation, $Da = 2$.

Five Term Expansion, $Da = 10$



- Five term expansion, $Da = 10$.

Five Term Expansion, $Da = 100$



- Five term expansion, $Da = 100$.

Dissociation Phase

- The expansion in the dissociation phase is:

$$B_0(t) = \frac{e^{-k\tau}}{\alpha},$$

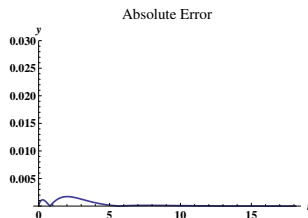
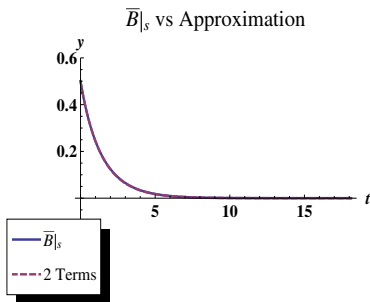
$$B_1(t) = -\frac{Dae^{-2k\tau}(-1 + e^{k\tau})\bar{h}q}{\alpha^2}$$

$$\tau = (1 + \omega_1 + \omega_2 + \dots)t$$

$$\omega_1 = -Da\bar{h}q,$$

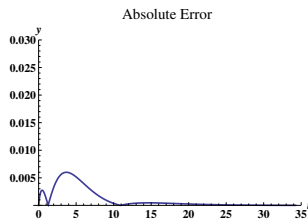
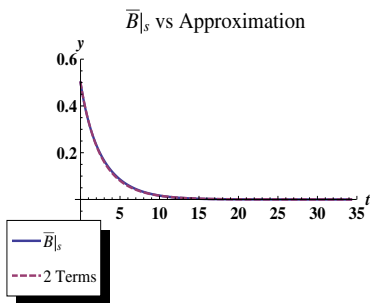
$$\omega_2 = Da\bar{h}q(-1 + q + Da\bar{h}q).$$

Two Term Expansion, $Da = 1/2$



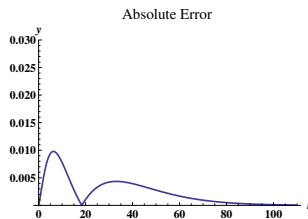
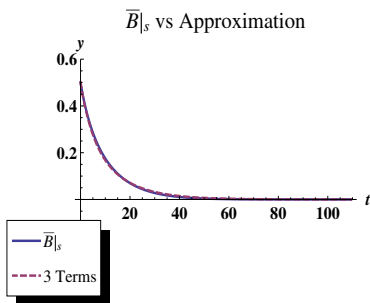
- Two term expansion, $Da = 1/2$.

Three Term Expansion, $Da = 2$



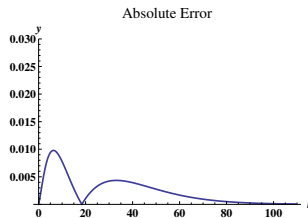
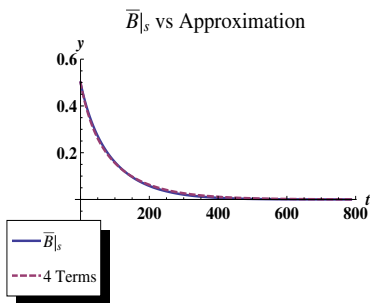
- Three term Approximation, $Da = 2$.

Five Term Expansion, $Da = 10$



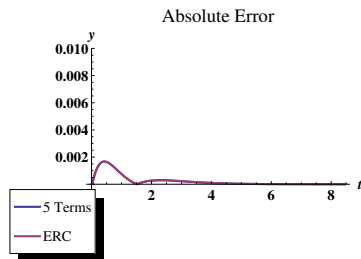
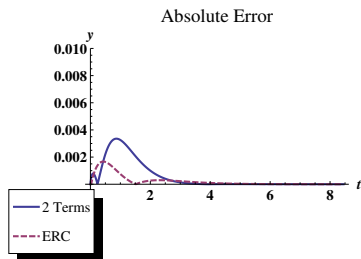
- Five term expansion, $Da = 10$.

Five Term Expansion, $Da = 100$



- Five term expansion, $Da = 100$.

Matches Up With ERC Approximation



- Left: Two term approximation vs ERC Approximation. Right: Five-Term approximation vs ERC Approximation.

Conclusions

- Modeling Multiple-Components in Optical Biosensors.
 - We must consider transport.
 - Full model simplifies to a coupled system of integrodifferential equations.
 - These equations further reduce to a set of nonlinear ODE's.
 - Formally holds for $Da \ll 1$, numerically everywhere.
- Sensogram Issues
 - Multiple reacting species make interpreting Sensogram data difficult.
 - Can fix this in certain cases by varying of C_1 .

Conclusions

- Single-Component Reactions
 - Strongly nonlinear problem when $Da = O(1)$.
 - Can find analytic approximations to \bar{B} by applying a homotopy method.
 - Must use a strained time scale.
 - Matches up with ERC approximations.

Future Work

- Tie together multiple-receptor and multiple-ligand model.
- Nonuniform initial receptor concentration.
- Helical geometries.

References

- 1 C. Bertucci, A. Piccoli, and M. Pistozzi Optical biosensors as a tool for early determination of absorption of lead candidates and drugs. *comb. chem. high throughput screen*, 10:433:440, 2007
- 2 D. A. Edwards. Transport effects on surface reaction arrays: biosensor applications. *Mathematical Biosciences*. 12-22,2007
- 3 E.F.Grabowski, L.I. Friedman, and E.F. Leonard. Effects of shear rate on diffusion and adhesion of blood platelets to a foreign surface. *Ind. Eng. Chem. Fund*, 11:224-232, 1972
- 4 J. He. The homotopy perturbation technique. *Computer Methods in Applied Mechanics and Engineering*, 178 (3):257-262, 1999
- 5 R.L. Rich, D. G. Myszka, Survey of the Year 2009 Commercial optical biosensor literature. *J. Mol. Recognit*, 24:892-914,2011

The End

Thanks for Coming! Questions?